

Informatyka

Zmień przedmiot ▾

E-podręczniki

Moduły

Informacja

Strona zapisana (wersja 2).

Implicit method Brak plików do pobrania.

In the implicitly called "backward Euler" method, used to solve non-stationary problems, the differential operator describing the "physics" of the modeled phenomenon is calculated in the "current" instant of time.

$$\frac{u_{t+1} - u_t}{dt} - \mathcal{L}(u_{t+1}) = f_{t+1}$$

So at each time step it is necessary to solve the equation for the next state u_{t+1} .

Let us follow the operation of the backward Euler method in the case of the isogeometric finite element method.

To develop a solver that uses the method implicitly in the isogeometric finite element method, we need to transform a strong formulation into a weak formulation.

So we multiply our equation by the test functions $(u_{t+1}, w) - (dt * \mathcal{L}(u_{t+1}), w) = (u_t + dt * f_{t+1}, w)$

We will use a linear combination of the B-spline function to approximate the state of our system at a given moment in time. For this purpose, we select the basis of two-dimensional B-spline functions, specifying the node vectors in the direction of the axis of the coordinate system, for example, the two-dimensional basis of the second-order B-spline function

$$\{B_{i,2}^x(x)B_{j,2}^y(y)\}_{i=1,\dots,N_x;j=1,\dots,N_y} u_{i,j}$$

They will be used to approximate the simulated scalar field of the current time instant

$$u(x, y; t) \approx \sum_{i=1,\dots,N_x;j=1,\dots,N_y} u_{i,j}^t B_i^x(x) B_j^y(y)$$

Similarly, we'll use the B-spline base functions for testing:

$$w(x, y) \in \{B_k^x(x)B_l^y(y)\}_{k=1,\dots,N_x; l=1,\dots,N_y} w^{k,l}$$

Assuming the differential operator \mathcal{L} describing "physics" is linear, our equation now looks like this:

$$\sum_{i=1,\dots,N_x; j=1,\dots,N_y} u_{i,j}^{t+1} (B_i^x(x)B_j^y(y) - dt * \mathcal{L}(B_i^x(x)B_j^y(y)), B_k^x(x)B_l^y(y)) = RHS.$$

$$\forall k = 1, \dots, N_x; l = 1, \dots, N_y$$

problem here, the conclusions presented here refer to any physical problem that can be simulated with the method described.

For example, for the problem of heat transport we have

$$\sum_{i=1,\dots,N_x; j=1,\dots,N_y} u_{i,j}^{t+1}$$

$$(B_i^x(x)B_j^y(y) - dt * \left(\frac{\partial^2(B_i^x(x)B_j^y(y))}{\partial x^2} + \frac{\partial^2(B_i^x(x)B_j^y(y))}{\partial y^2} \right), B_k^x(x)B_l^y(y)) = RHS$$

$$\forall k = 1, \dots, N_x; l = 1, \dots, N_y$$

Thanks to the weak wording, we can integrate by parts

$$\sum_{i=1,\dots,N_x; j=1,\dots,N_y} u_{i,j}^{t+1}$$

$$\left((B_i^x(x)B_j^y(y), B_k^x(x)B_l^y(y)) - dt * \left(\frac{\partial(B_i^x(x)B_j^y(y))}{\partial x}, \frac{\partial(B_k^x(x)B_l^y(y))}{\partial x} \right) - dt * \left(\frac{\partial(B_i^x(x)B_j^y(y))}{\partial y}, \frac{\partial(B_k^x(x)B_l^y(y))}{\partial y} \right) \right) = RHS$$

$$\forall k = 1, \dots, N_x; l = 1, \dots, N_y$$

Due to the structure of the tensor product of the B-spline function and due to the fact that the derivative in the y direction of the B-spline in the x-axis direction gives 0 (because these functions are constant in the y-axis direction) and similarly for the derivative in the y-direction of the B-spline in the x-axis direction the x axis we have

$$\sum_{i=1,\dots,N_x; j=1,\dots,N_y} u_{i,j}^{t+1}$$

$$\left((B_i^x(x)B_j^y(y), B_k^x(x)B_l^y(y)) - dt * \left(\frac{\partial B_i^x(x)}{\partial x} B_j^y(y), \frac{\partial B_k^x(x)}{\partial x} B_l^y(y) \right) - dt * \left(B_i^x(x) \frac{\partial B_j^y(y)}{\partial y}, B_k^x(x) \frac{\partial B_l^y(y)}{\partial y} \right) \right) = RHS$$

$$\forall k = 1, \dots, N_x; l = 1, \dots, N_y$$

Note that our system of equations to solve is

$$(M_x \otimes M_y - dt * S_x \otimes M_y - dt * M_x \otimes S_y) u^{t+1} = F(t)$$

where

$\{M_x \otimes M_y\}_{i,j,k,l} = \int B_i^x(x) B_k^x(x) B_j^y(y) B_l^y(y) = \int B_i^x(x) B_j^y(y) B_k^x(x) B_l^y(y) = \mathbf{M}_{i,j,k,l}$ is a mass matrix which is a Kronecker product of two one-dimensional mass matrices,

$\{S_x \otimes M_y\}_{i,j,k,l} = \int \frac{\partial B_i^x(x)}{\partial x} \frac{\partial B_k^x(x)}{\partial x} B_j^y(y) B_l^y(y) = \int \frac{\partial B_i^x(x)}{\partial x} B_j^y(y) \frac{\partial B_k^x(x)}{\partial x} B_l^y(y)$ is the Kronecker product of the one-dimensional stiffness matrix and the one-dimensional mass matrix, and

$\{M_x \otimes S_y\}_{i,j,k,l} = \int B_i^x(x) B_k^x(x) \frac{\partial B_j^y(y)}{\partial y} \frac{\partial B_l^y(y)}{\partial y} = \int B_i^x(x) \frac{\partial B_j^y(y)}{\partial y} B_k^x(x) \frac{\partial B_l^y(y)}{\partial y}$ is the Kronecker product of the one-dimensional mass matrix and the one-dimensional stiffness matrix.

Each of these matrices can be factored in linear time using the variable-directional solver algorithm. However, it is no longer possible to factorize their sum in linear time. This is possible only when we introduce a time step scheme that allows the matrix to be separated into sub-matrices in time sub-steps so that the factorization cost remains linear.

The Peaceman-Rachford diagram allows to split the time step into two sub-steps

$$(M_x \otimes M_y - dt * S_x \otimes M_y) u^{t+1/2} = F(t + 1/2) + (dt * M_x \otimes S_y) u^t$$

$$(M_x \otimes M_y - dt * M_x \otimes S_y) u^{t+1} = F(t + 1/2) + (dt * S_x \otimes M_y) u^{t+1/2}$$

where we can merge the left side matrices into a single matrix with a Kronecker product structure that can be factored in linear time using the variable direction solver algorithm

$$(M_x - dt * S_x) \otimes M_y u^{t+1/2} = F(t + 1/2) + (dt * M_x \otimes S_y) u^t$$

$$M_x \otimes (M_y - dt * S_y) u^{t+1} = F(t + 1/2) + (dt * S_x \otimes M_y) u^{t+1/2}$$

The right hand function here represents the changes caused by the force acting on the system during the time step. It is the sum of two elements:

1. The state of our system at the previous moment in time $(u_t, w) = \sum_{i=1,\dots,N_x; j=1,\dots,N_y} u_{i,j}^t (B_i^x(x) B_j^y(y), B_k^x(x) B_l^y(y))$ (also multiplied by the test function and area integrated). Of course, we also use a linear combination of B-spline base functions to represent the state of our system in the previous time step

$$u(x, y; t) = u_t = \sum_{i=1,\dots,N_x; j=1,\dots,N_y} u_{i,j}^t B_i^x(x) B_j^y(y)$$

2. Changes caused by a force acting on the system during the time step $(f_{t+1}, w) = (f_{t+1}(x, y), B_k^x(x) B_l^y(y))$

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